

# SIMS 2015 Plenary



## Accomplishing Ground Moving Innovations through Modeling, Simulation, and Optimal Control

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**LiU** EXPANDING REALITY

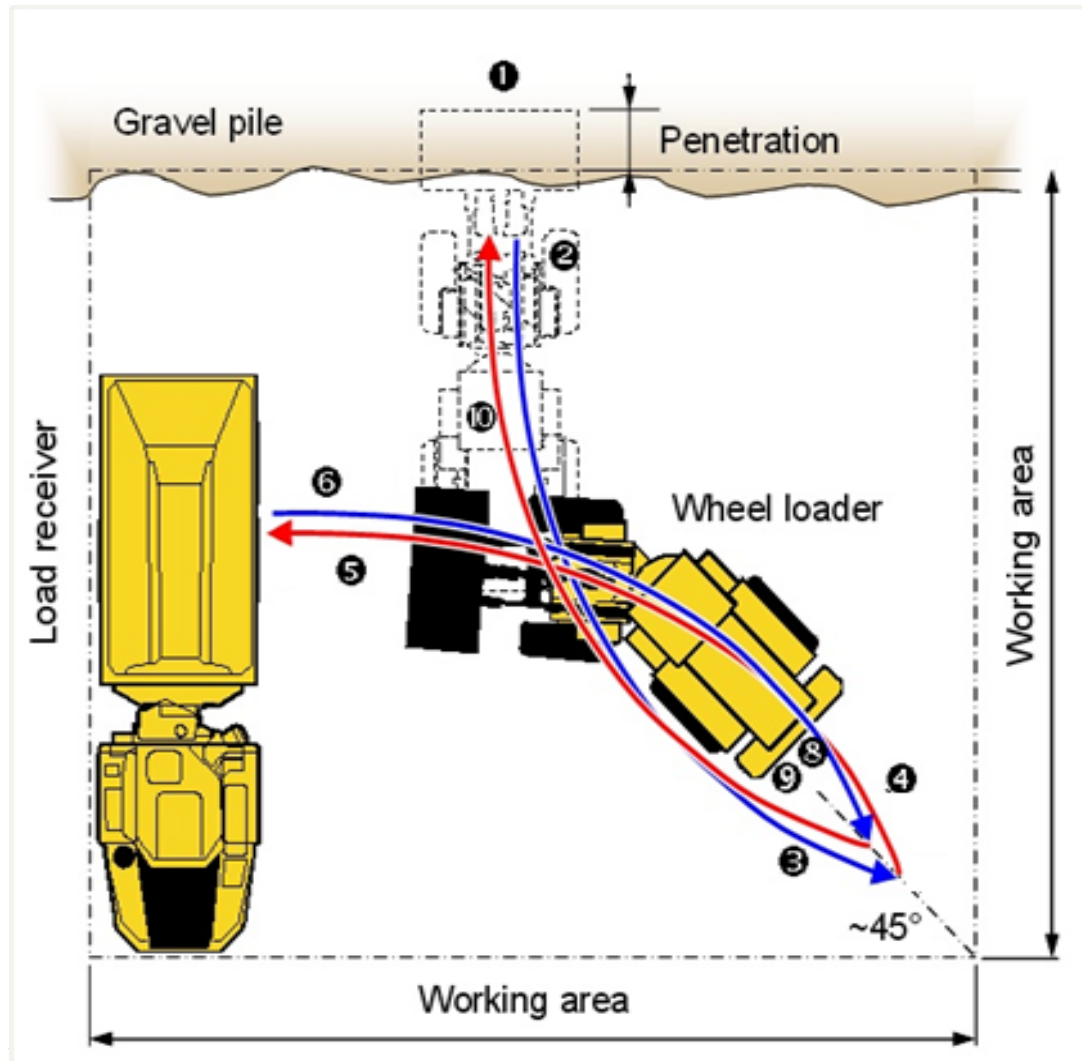
# The Application

## Big Toys for Big Boys



# The Application

## Short Loading Cycle



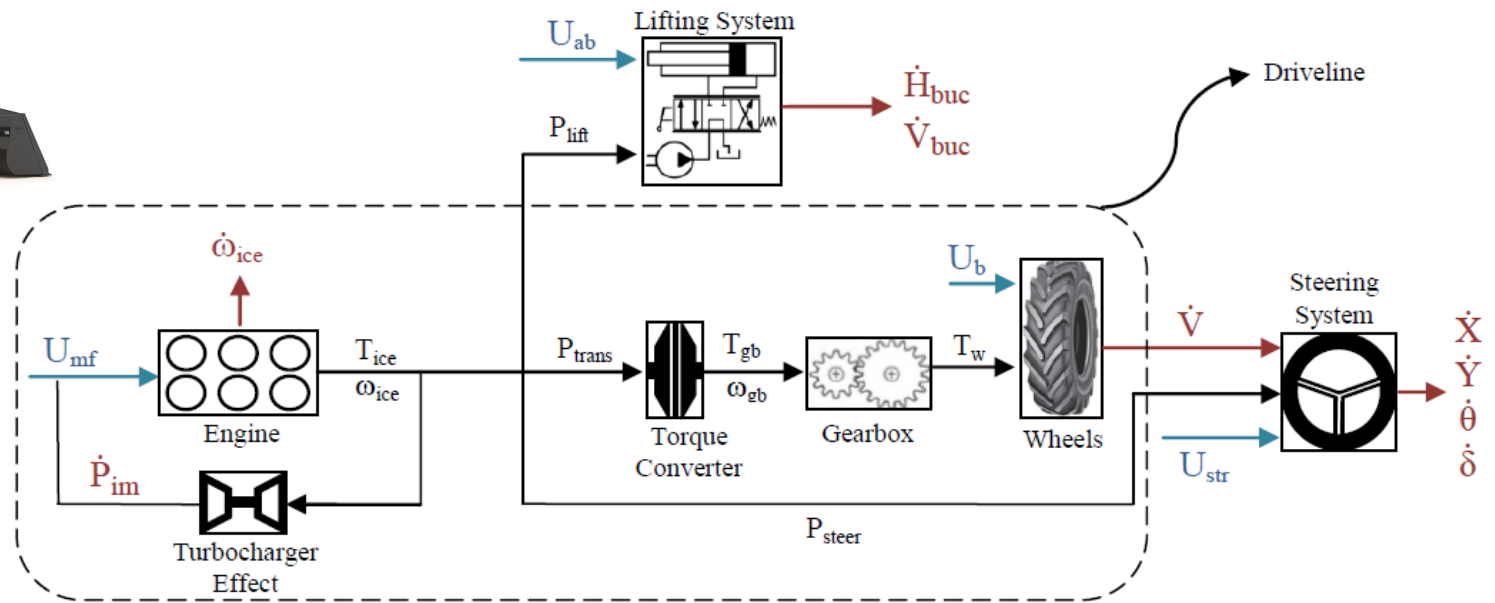
- Pick up gravel
- Reverse and lift
- Stop
- Drive and lift
- Empty bucket
- Reverse and lower
- Stop
- Drive
- Fill Bucket

-How to drive optimally?

# Outline

- Wheel loader application
  - How to operate the wheel loader optimally
  - Modeling for control and optimal control
- Formulating and solving the optimal control problem
  - Numerical optimal control
- Design problems and trade-offs
  - Solving fuel and time optimal driving
  - Design case – Stiff converter
  - Design case – Intelligent braking
  - Design case – Where to park load receiver?
- Conclusions

# Wheel loader model



*Sub systems :*

## 1- Driveline

**Controls:** Fuel injection, Brake torque signal.

**States:** Engine speed, Intake manifold pressure, Vehicle speed.

## 2- Lifting system

**Controls:** Bucket lift acceleration.

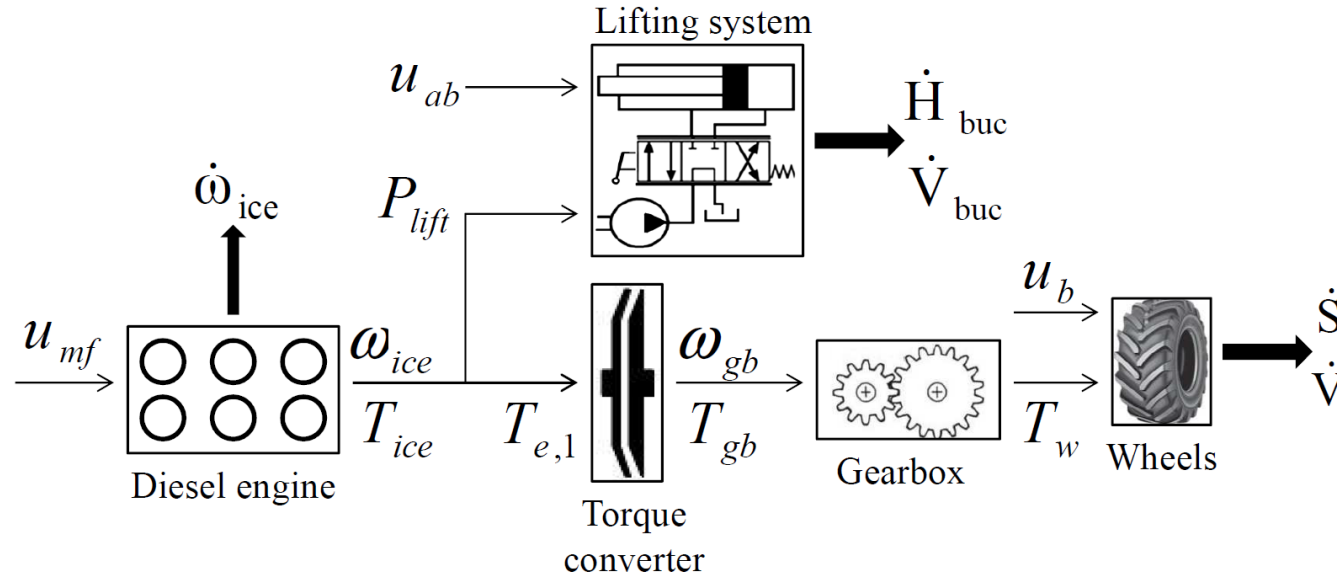
**States:** Bucket height, Bucket lift speed.

## 3- Steering system

**Controls:** Derivative of steering angle.

**States:** Vehicle position  $X$  &  $Y$ , Heading angle, Steering angle.

# Wheel loader model



$$\text{States: } \begin{Bmatrix} \omega_{ice} \\ S \\ V \\ H_{bucket} \\ V_{bucket} \end{Bmatrix} = \begin{Bmatrix} \text{Engine speed} \\ \text{Travelled distance} \\ \text{Vehicle speed} \\ \text{Lift height} \\ \text{Lift speed} \end{Bmatrix}$$

$$\text{Controls: } \begin{Bmatrix} U_{mf} \\ U_{ab} \\ U_b \end{Bmatrix} = \begin{Bmatrix} \text{Fuel} \\ \text{Bucket acceleration} \\ \text{Braking torque} \end{Bmatrix}$$

$$\frac{d\omega_{ice}}{dt} = \frac{1}{J_{ice}} \left( T_{ice}(U_{mf}, \omega_{ice}) - \frac{P_{load}(V_{buc}, V)}{\omega_{ice}} \right) \quad (1)$$

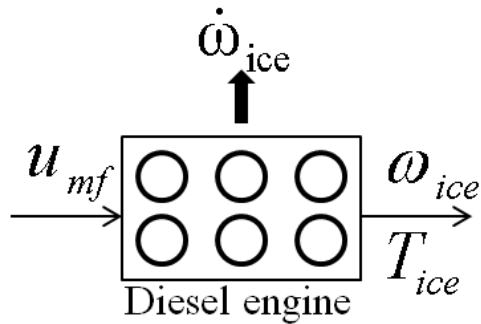
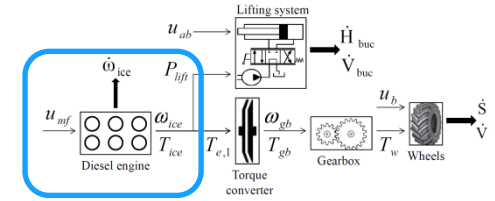
$$\frac{dS}{dt} = V \quad (2)$$

$$\frac{dV}{dt} = \frac{\text{sign}(\gamma) (F_{trac}(U_b, \omega_{ice}) - F_{roll})}{M_{tot}} \quad (3)$$

$$\frac{dH_{buc}}{dt} = V_{buc} \quad (4)$$

$$\frac{dV_{buc}}{dt} = U_{ab} \quad (5)$$

# Diesel engine model



$$T_{ice} = T_{ig} - T_{fric}$$

$$\eta_{ig} = \eta_{ig,ch} \left( 1 - \frac{1}{r_c^{\gamma_{cyl}-1}} \right)$$

$$T_{ig} = \frac{\eta_{ig} q_{hv} n_{cyl} U_{mf} 10^{-6}}{2 \pi n_r}$$

$$T_{fric} = \frac{V_d 10^5}{4 \pi} \left( c_{fr1} \omega_{ice}^2 + c_{fr2} \omega_{ice} + c_{fr3} \right)$$

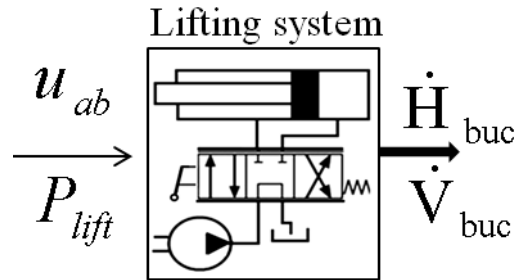
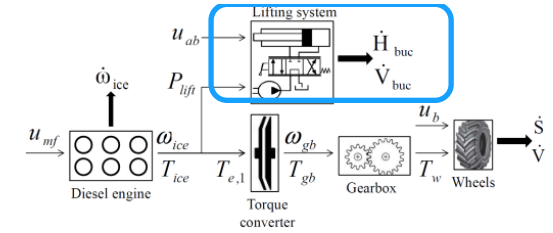
$$\dot{m}_f = \frac{10^{-6}}{4 \pi} U_{mf} \omega_{ice} n_{cyl}$$

$$P_{load} = P_{trac} + P_{lift}$$

$$\frac{d\omega_{ice}}{dt} = \frac{1}{J_{ice}} \left( T_{ice}(U_{mf}, \omega_{ice}) - \frac{P_{load}(V_{buc}, V)}{\omega_{ice}} \right) \quad (1)$$



# Lift system and constraints



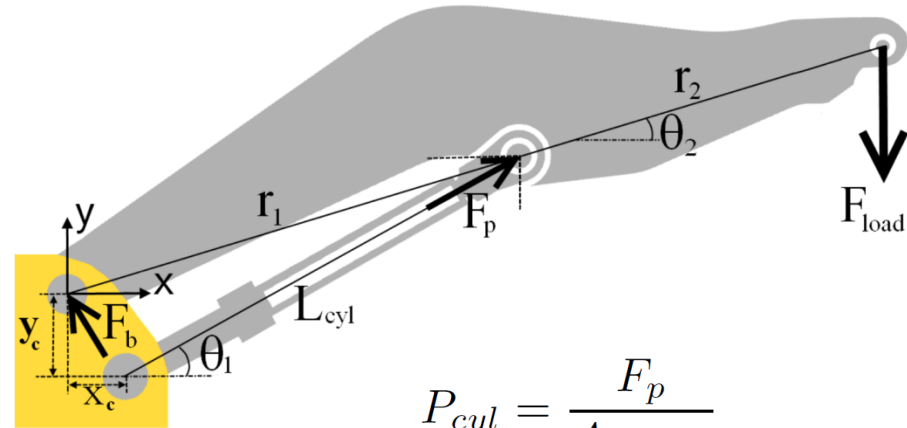
$$F_{load} = M_{buc} (g + U_{ab})$$

$$P_{lift,net} = F_{load} V_{buc}$$

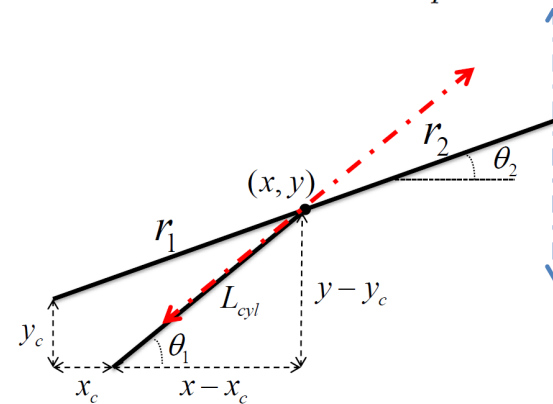
$$P_{lift} = \frac{(1 + C_{loss}) P_{lift,net}}{\eta_{lift}}$$

$$\frac{dH_{buc}}{dt} = V_{buc} \quad (4)$$

$$\frac{dV_{buc}}{dt} = U_{ab} \quad (5)$$



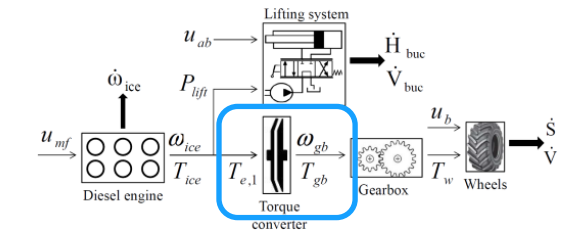
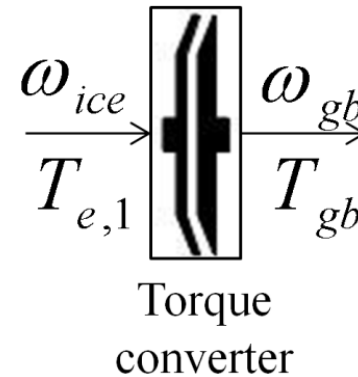
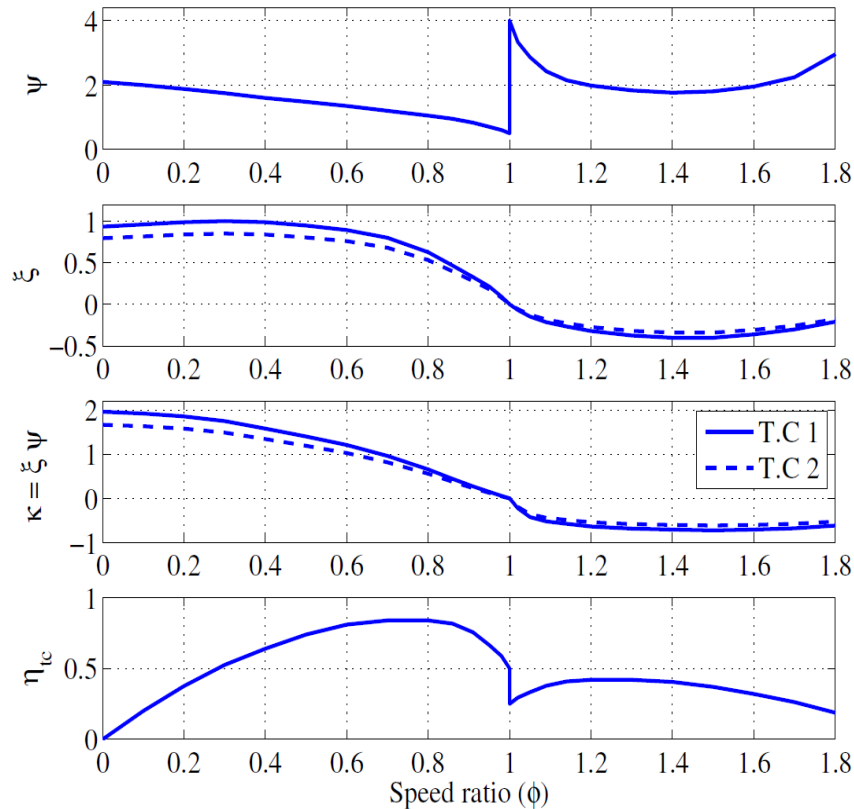
$$P_{cyl} = \frac{F_p}{A_{piston}}$$



$$V_{lift,max} = k(\theta_2) v_{pist,max}$$



# Torque converter



$$\phi = \frac{|\text{gearbox speed}|}{\omega_{ice}}$$

$$\eta_{tc} = \begin{cases} \phi \cdot \psi & \phi \leq 1 \\ \frac{1}{\phi \cdot \psi} & \phi > 1 \end{cases}$$

$$\kappa(\phi) = \psi(\phi) \xi(\phi)$$

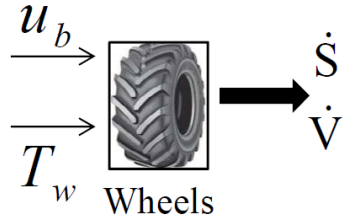
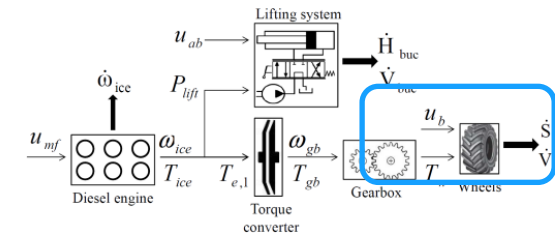
$$T_{e,1} = \xi(\phi) \left( \frac{\omega_{ice}}{1000} \right)^2$$

$$T_{gb} = \kappa(\phi) \left( \frac{\omega_{ice}}{1000} \right)^2 | \text{sign}(\gamma) |$$

$$P_{trac} = T_{e,1} \omega_{ice}$$

- 2 T.C. studied (one delivers 15 % more torque)
- Remove the discontinuities (efficient numerical optimization)
  - Differentiable model

# Vehicle speed and position



$$F_{trac} = \frac{T_w - \text{sign}(V) T_b}{r_w}$$

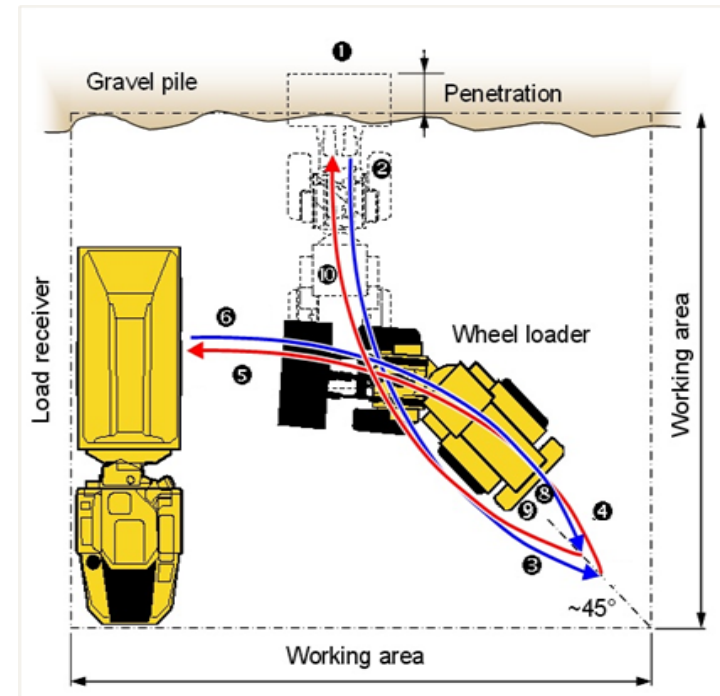
$$F_{roll} = c_r (M_{veh} + M_{buc}) g$$

$$T_w = T_{gb} \eta_{gb} \gamma$$

$$T_b = U_b$$

$$\frac{dS}{dt} = V$$

$$\frac{dV}{dt} = \frac{\text{sign}(\gamma) (F_{trac}(U_b, \omega_{ice}) - F_{roll})}{M_{tot}}$$



(2)

(3)

# Steering system and vehicle position

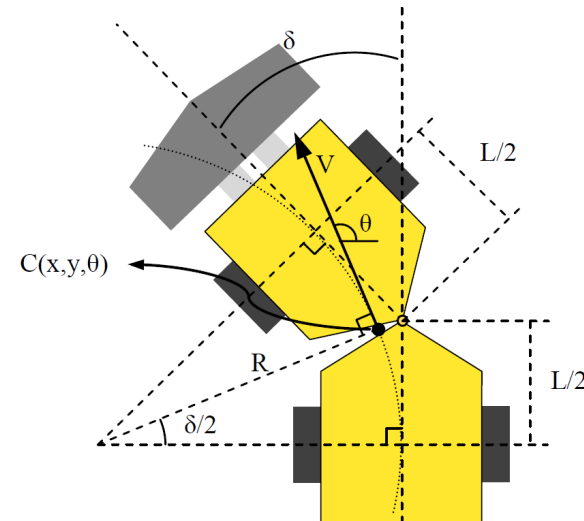
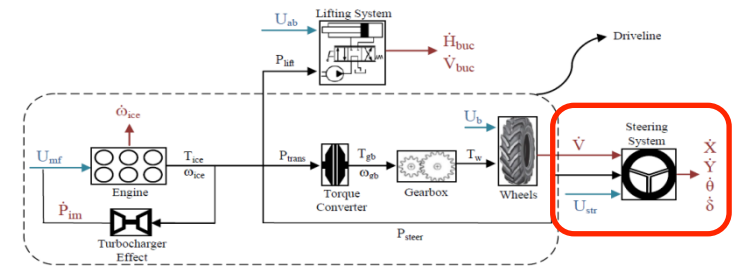
$$P_{\text{steer}} \propto \text{Derivative of steering angle } U_{\text{str}}^2$$

$$\frac{d\delta}{dt} = U_{\text{str}}$$

$$\frac{d\theta}{dt} = \frac{V}{R}$$

$$\frac{dX}{dt} = V \cos(\theta)$$

$$\frac{dY}{dt} = V \sin(\theta)$$



*Constraints during steering*

*Continuous steering angle*

$$U_{\text{str,min}} \leq U_{\text{str}} \leq U_{\text{str,max}}$$

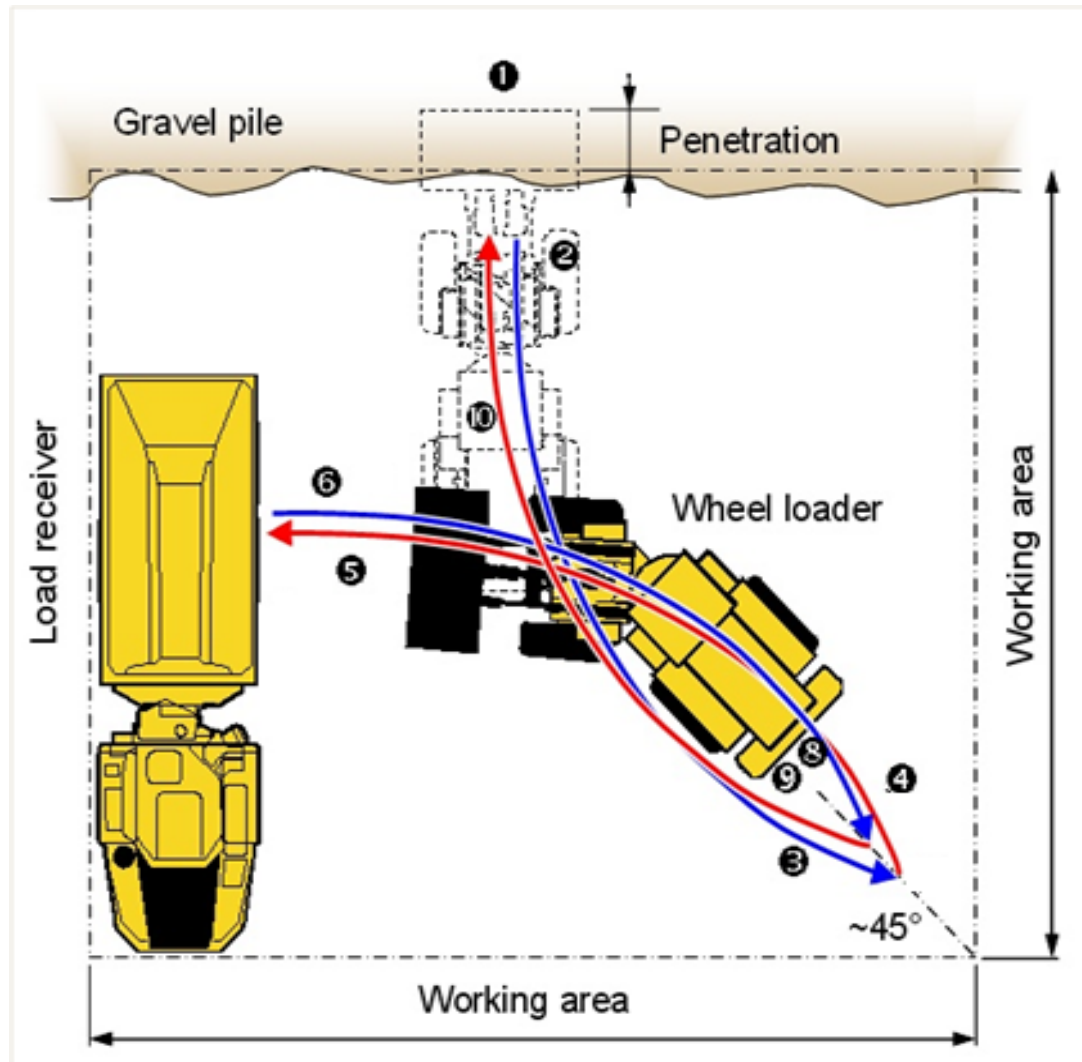
*Minimum turning radius*

$$R_{\text{min}} \leq \frac{L}{2 \tan(\frac{\delta}{2})} = R$$

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# How to drive optimally?



Lift transport section (and complete cycle)

- Minimum Time
- Minimum Fuel

# Optimal Control Problem

## Complete cycle – Fork lift application

$$\begin{aligned}
 & \min_{s(t), u(t), \gamma(t)} \quad T \quad \text{or} \quad M_f \\
 & \text{s.t.} \\
 & \quad \dot{s}(t) = f(s(t), u(t), \gamma(t)) \\
 & \quad u_{\min} \leq u(t) \leq u_{\max} \\
 & \quad s_{\min} \leq s(t) \leq s_{\max} \\
 & \quad R \leq R_{\max} \\
 & \quad T_{ice}(s(t), u(t)) \leq T_{ice, \max} \\
 & \quad p_{cyl}(s(t), u(t)) \leq p_{cyl, \max} \\
 & \quad s(0) = (120, 0, 0, 0, 1.1 \times 101300, \frac{\pi}{2}, 0, 0, 0) \\
 & \quad t \in [0, t_1] : \gamma(t) = 0, h_{lift}(t_1) = 0.2, \\
 & \quad t \in [t_1, t_2] : \gamma(t) = -60, \\
 & \quad t \in [t_2, t_3] : \gamma(t) = 0, v(t_3) = 0, \dot{v}_{\min} \leq |\dot{v}(t)|, \\
 & \quad t \in [t_3, t_4] : \gamma(t) = 60, h_{lift}(t_4) = h_{end}, \\
 & \quad t \in [t_4, t_5] : \gamma(t) = 0, u_{dstr}(t) = u_{ab}(t) = \delta(t) = v(t_5) = 0, \\
 & \quad \int_{t_4}^{t_5} v \, dt = L_p, (x, y)(t_5) = [x_e, y_e], \dot{v}_{\min} \leq |\dot{v}(t)|, \\
 & \quad t \in [t_5, t_6] : \gamma(t) = v(t) = 0, h(t_6) = h_{end} - 0.2, \\
 & \quad t \in [t_6, t_7] : \gamma(t) = -60, u_{ab}(t) = u_{dstr}(t) = \delta(t) = 0, \\
 & \quad \int_{t_6}^{t_7} v \, dt = -L_p, \\
 & \quad t \in [t_7, t_8] : \gamma(t) = -60, h_{lift}(t_8) = 0.2, \\
 & \quad t \in [t_8, t_9] : \gamma(t) = 0, u_{ab}(t) = v(t_9) = 0, \dot{v}_{\min} \leq |\dot{v}(t)|, \\
 & \quad t \in [t_9, t_{10}] : \gamma(t) = 60, u_{ab}(t) = 0, \\
 & \quad t \in [t_{10}, T] : \gamma(t) = 0, u_{ab}(T) = u_{dstr}(T) = u_b(T) = 0, \\
 & \quad s(T) = (-, 0, 0, 0, -, \frac{\pi}{2}, 0, 0, 0), \dot{v}_{\min} \leq |\dot{v}(t)|,
 \end{aligned}$$

# PROPT tool and model implementation



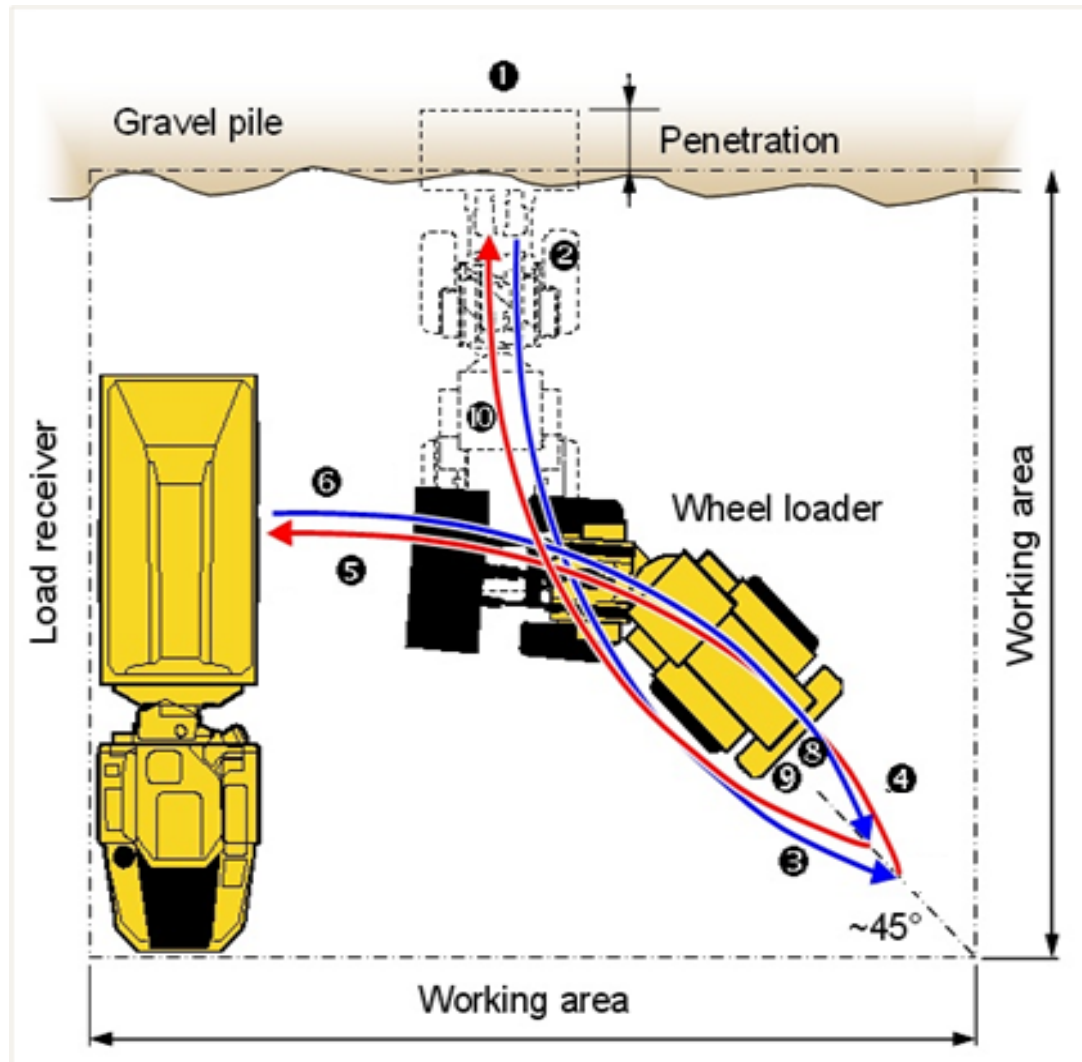
# Path to Efficient Solution

- Discretize state and controls in time  
Very large but sparse optimization problems
- Efficient solvers available  
IPOPT, SNOPT, KNITRO
- Efficient by using gradients and hessians.  
Use Algorithmic Differentiation
- Packages enable us to formulate problem and enter models that are differentiable.  
DIRCOL, ACADO, PROPT, CasADi, OpenModelica...
- Can now solve large non-linear problems efficiently

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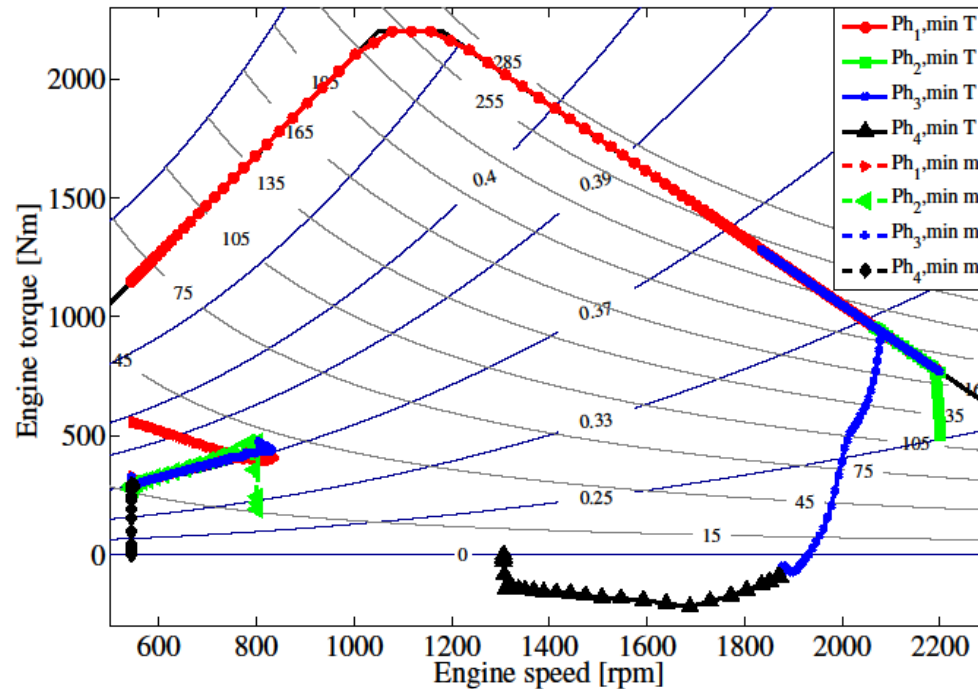
# How to drive optimally?



## Lift & transport section

- Minimum Time
- Minimum Fuel

# Time and fuel optimal solutions, trajectories

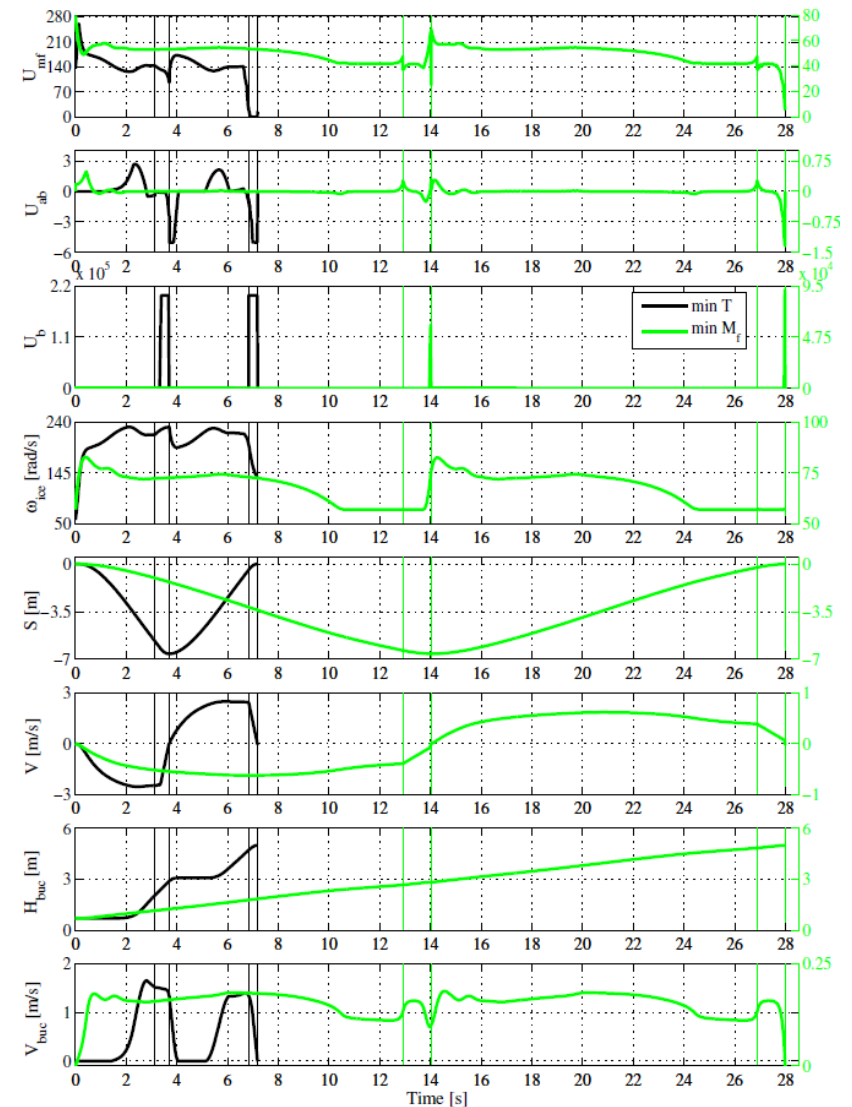


*Min T:*

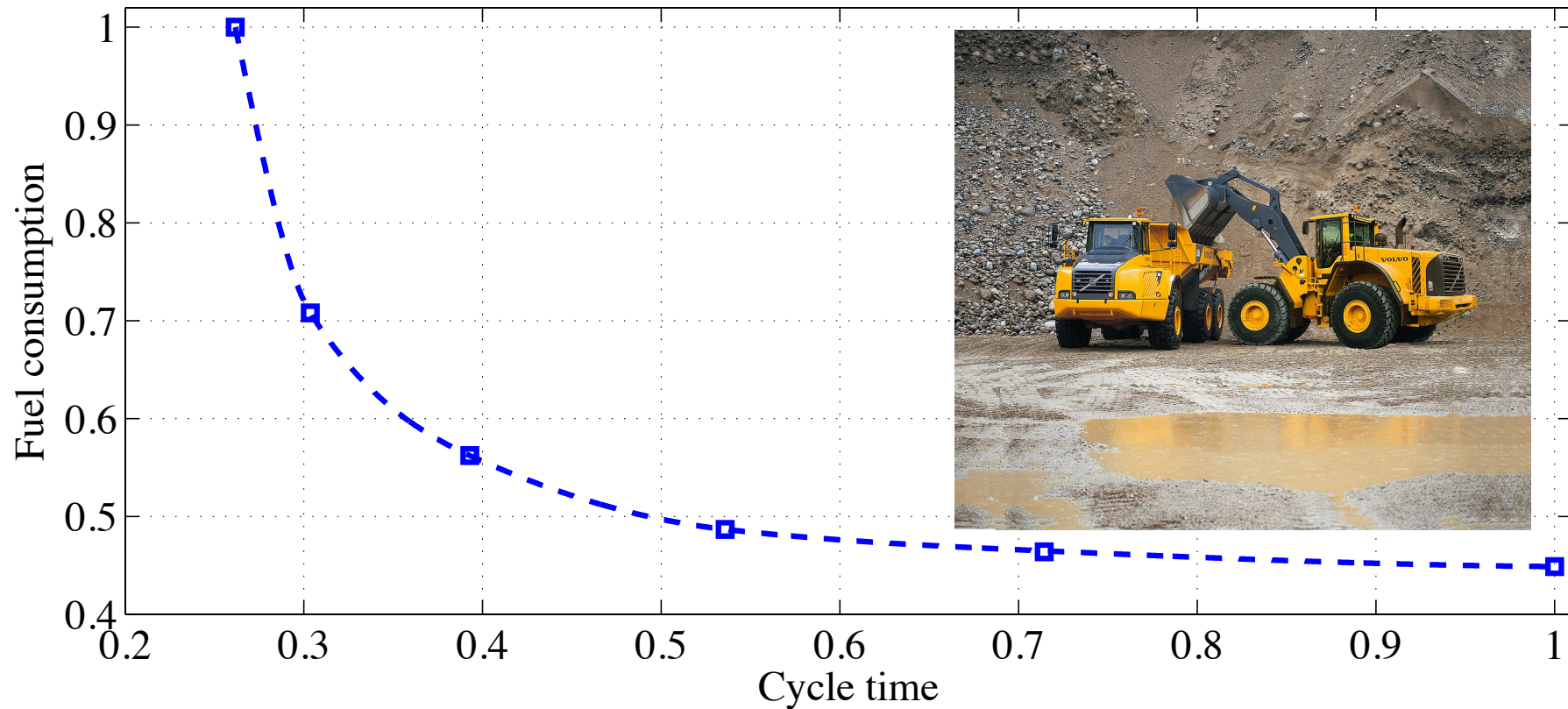
*acceleration » lifting » acceleration » lifting*

*Min Fuel:*

- Avoiding high engine speeds.
- Simultaneous acceleration and lifting

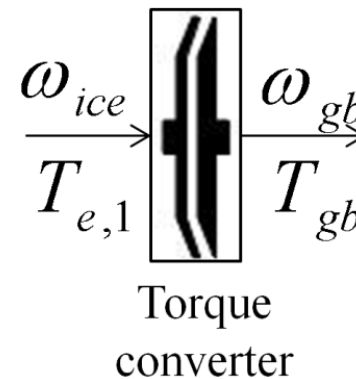
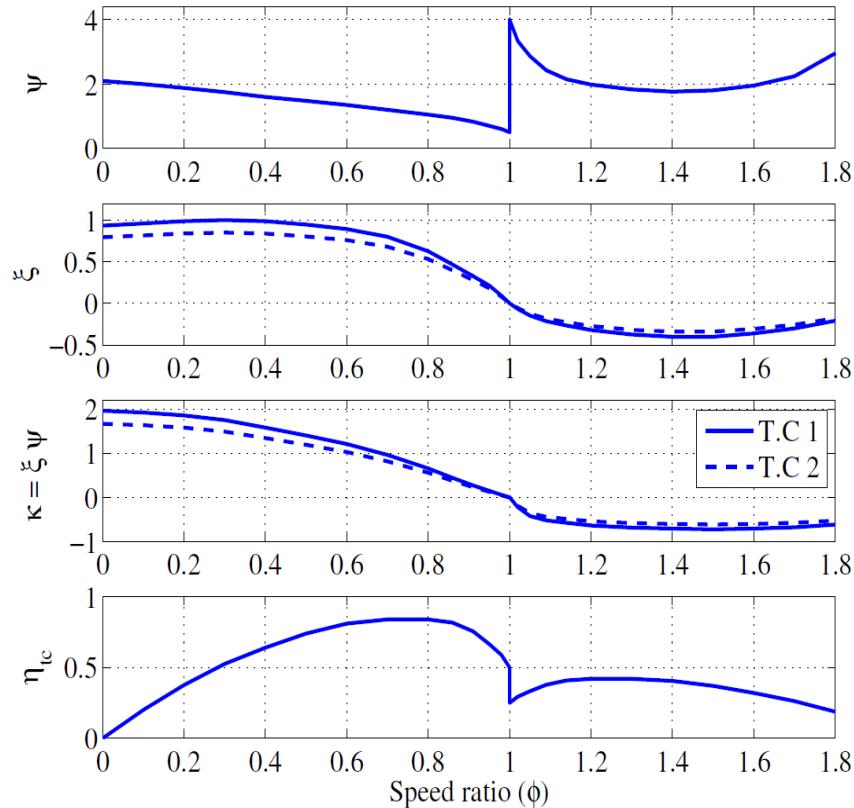
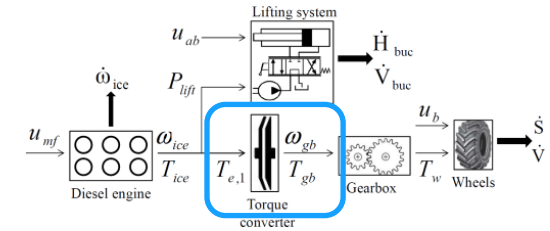


# Trade-off between fuel and time optimal



- Pareto front informative
  - Fuel optimal cycle 50 % shorter -> only 5 % fuel cost
  - Time optimal cycle 5 % longer -> 30 % fuel savings
- Total Cost Optimization
  - Site optimization

# Torque converter selection



$$\phi = \frac{|\text{gearbox speed}|}{\omega_{ice}}$$

$$\eta_{tc} = \begin{cases} \phi \cdot \psi & \phi \leq 1 \\ \frac{1}{\phi \cdot \psi} & \phi > 1 \end{cases}$$

$$\kappa(\phi) = \psi(\phi) \xi(\phi)$$

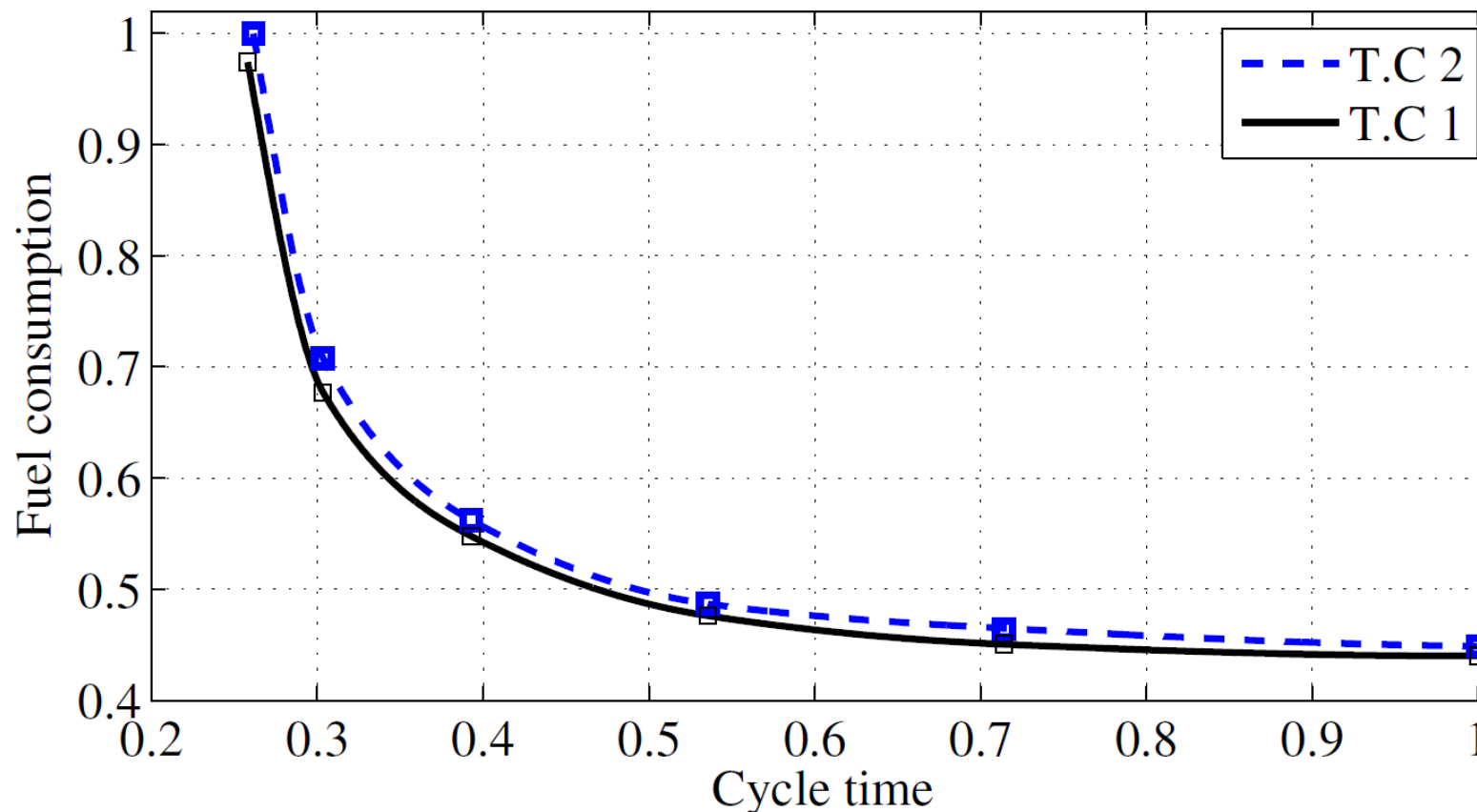
$$T_{e,1} = \xi(\phi) \left( \frac{\omega_{ice}}{1000} \right)^2$$

$$T_{gb} = \kappa(\phi) \left( \frac{\omega_{ice}}{1000} \right)^2 | \text{sign}(\gamma) |$$

$$P_{trac} = T_{e,1} \omega_{ice}$$

- 2 T.C. studied (one delivers 15 % more torque)
- No efficiency difference.

# Trade-off between fuel and time optimal

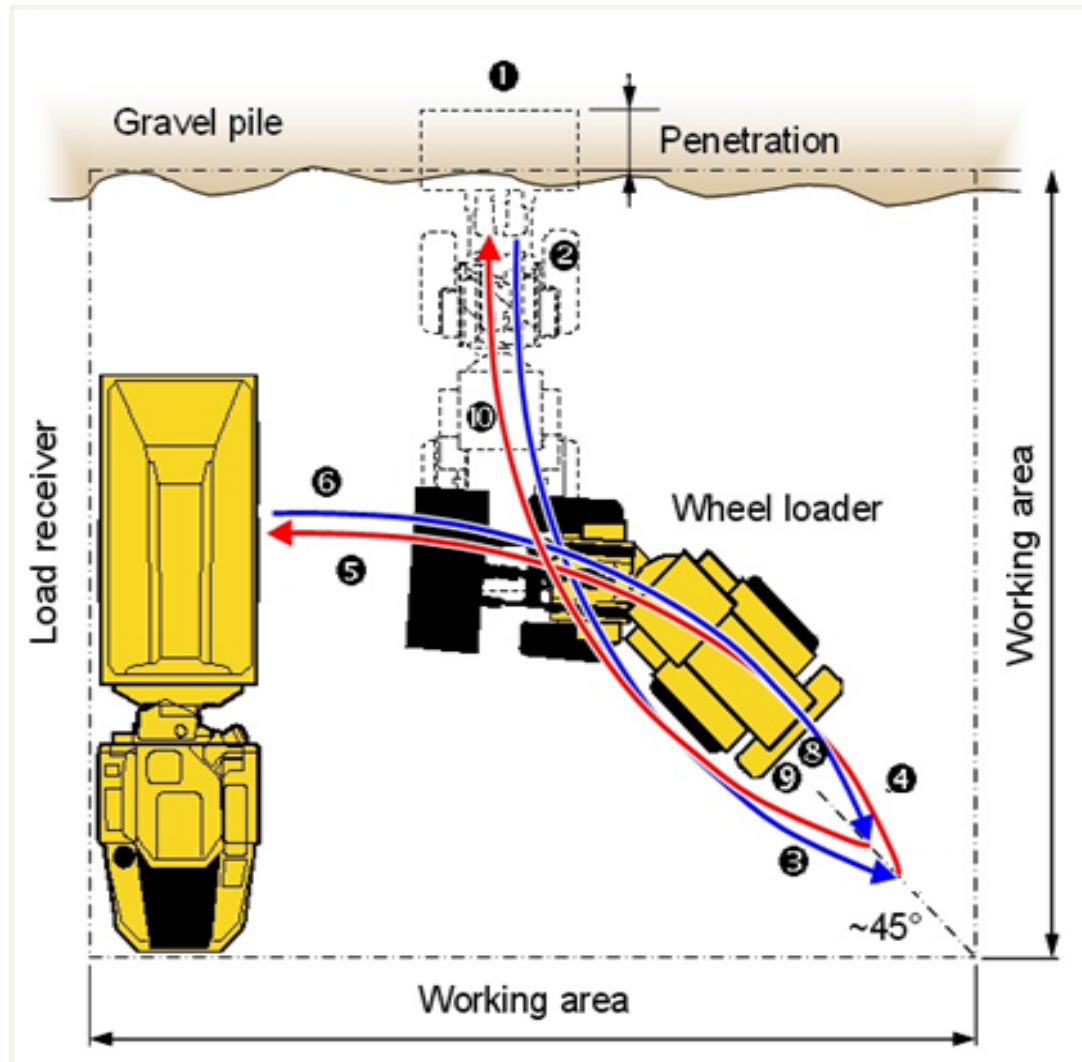


- Stiff torque converter is proven better – New knowledge
- Its a free lunch.
- In production = Innovation



# Intelligent Braking

## Torque Converter vs Service Brakes



Easy driving

- Switch to reverse
- Use engine and torque converter to brake

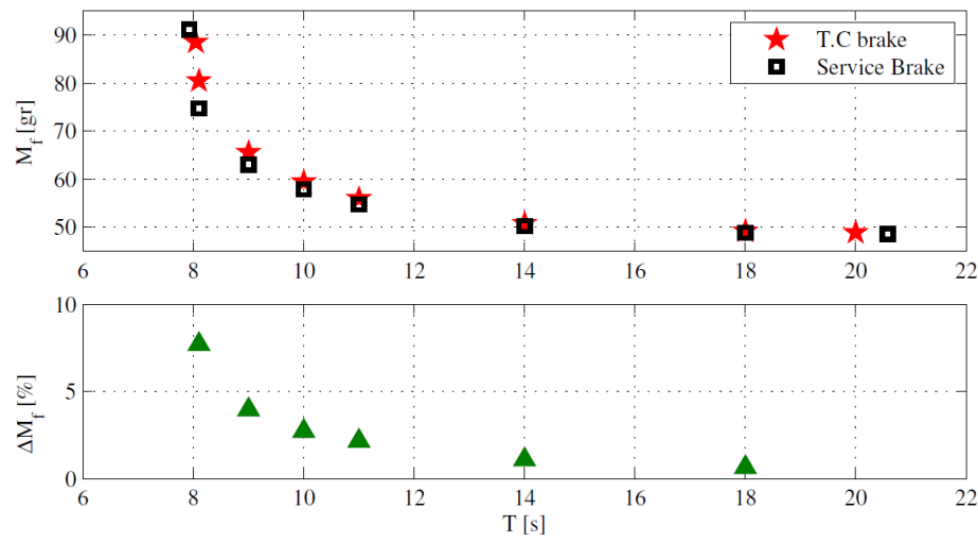
New idée:

- Switch to reverse
- Control service brakes

- How much is saved?

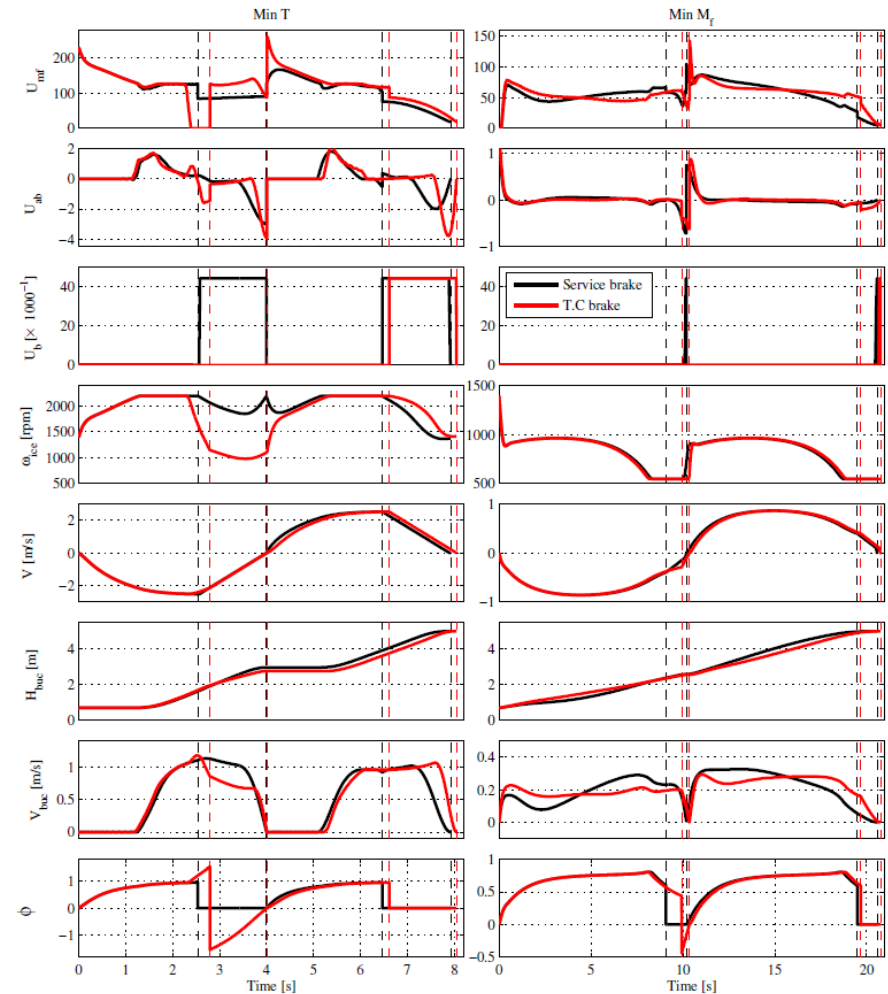
# Intelligent Braking

## Torque Converter vs Service Brakes

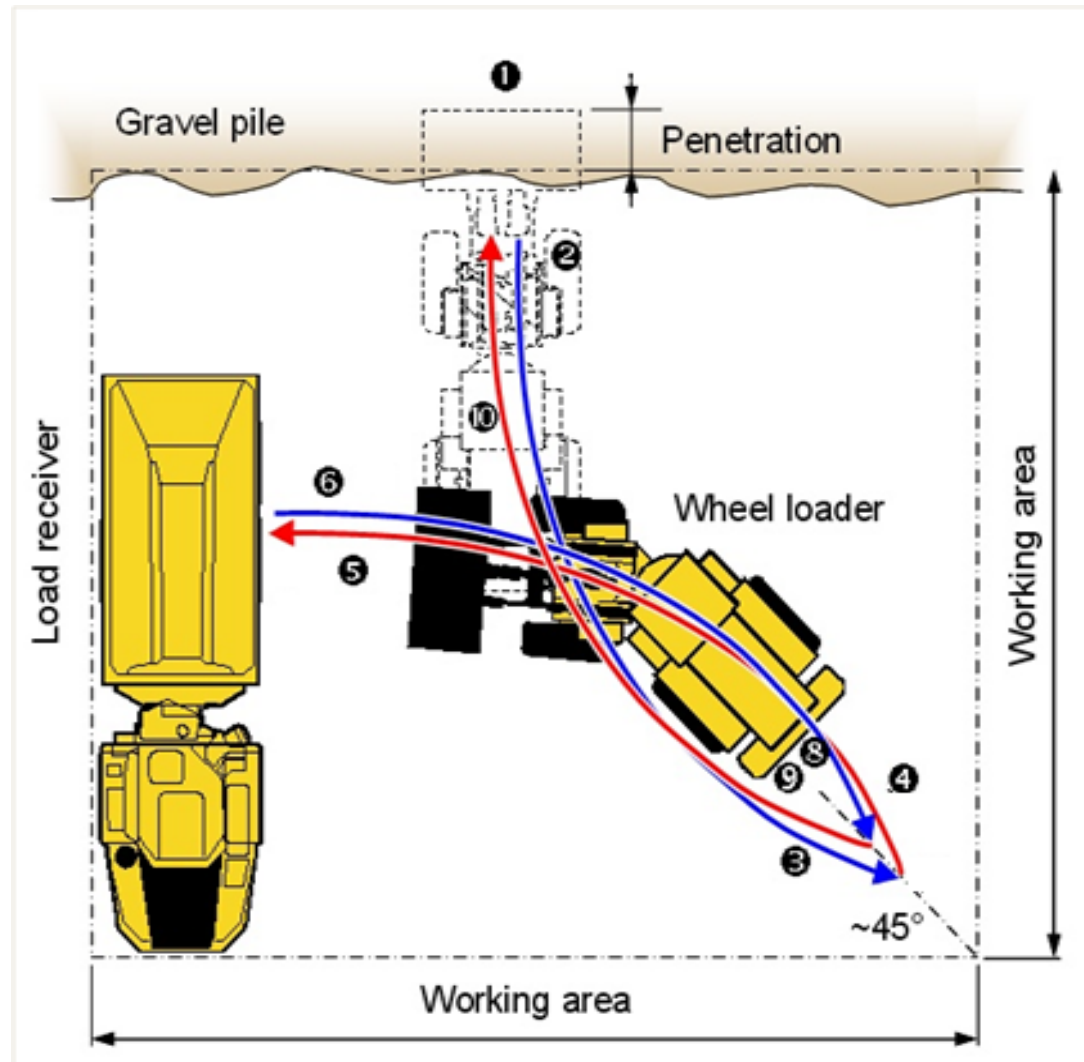


Intelligent braking is

- More efficient
- Faster
- In production = Innovation



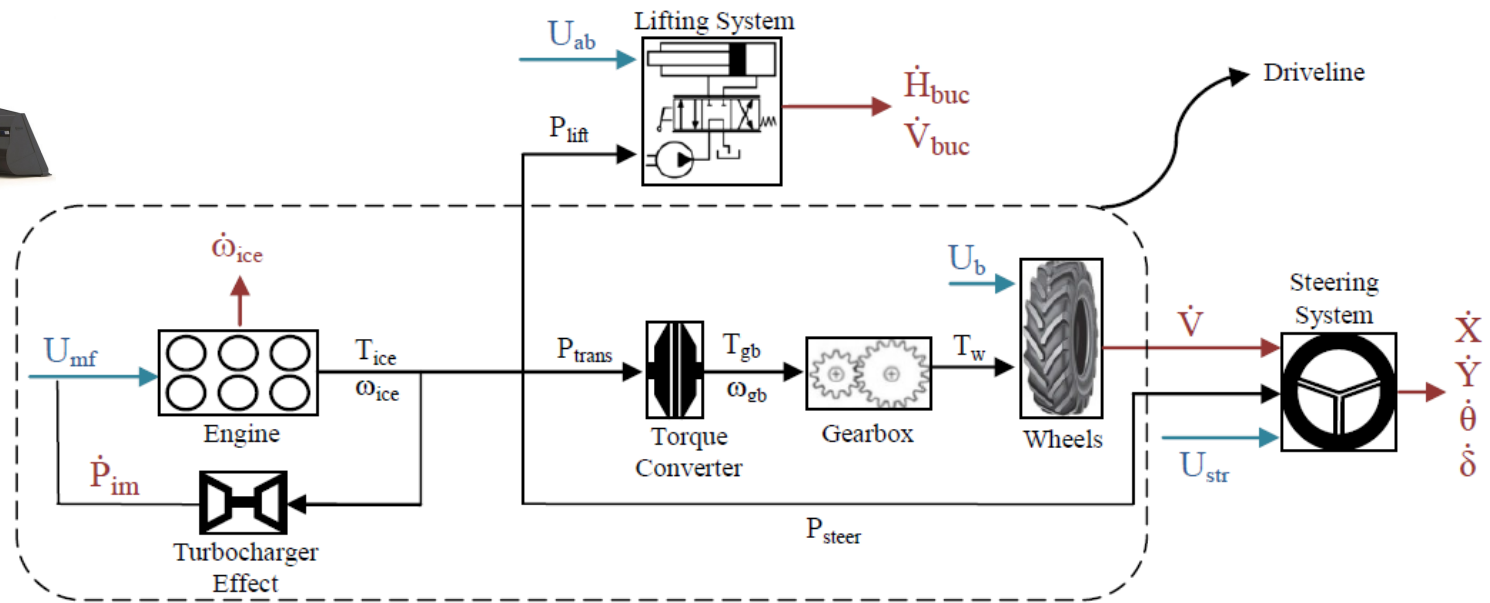
# Free Load Receiver Placement



Increased freedom

- Position
- Orientation

# Full Wheel Loader Model



*Sub systems :*

**1- Driveline**

**Controls:** Fuel injection, Brake torque signal.

**States:** Engine speed, Intake manifold pressure, Vehicle speed.

**2- Lifting system**

**Controls:** Bucket lift acceleration.

**States:** Bucket height, Bucket lift speed.

**3- Steering system**

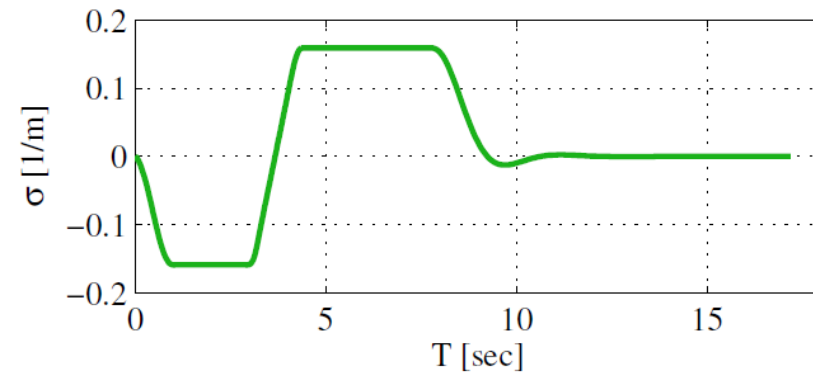
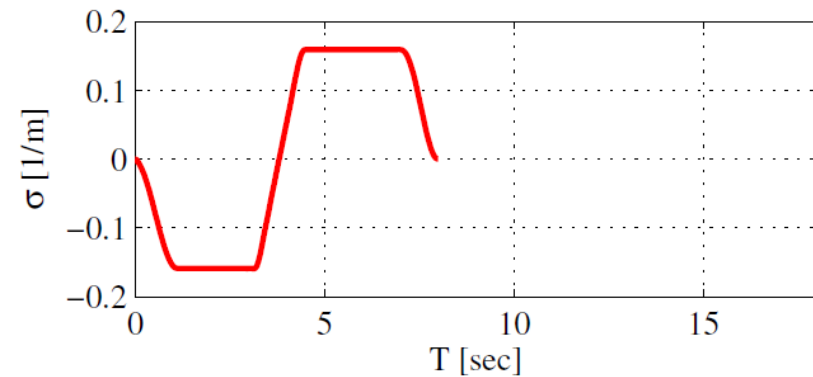
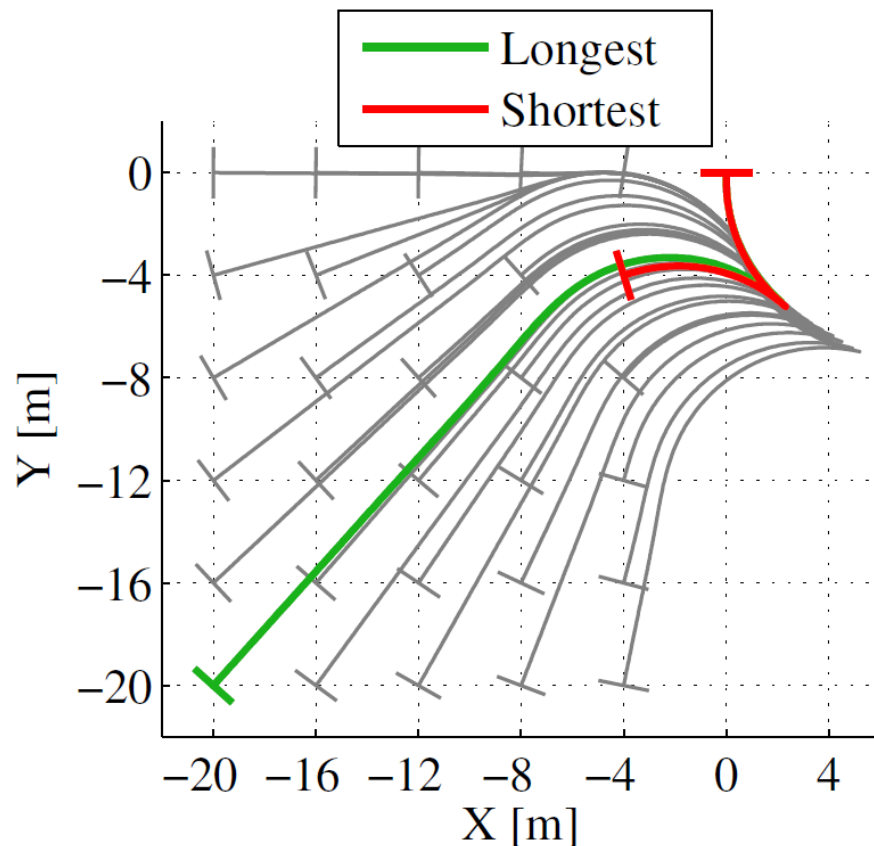
**Controls:** Derivative of steering angle.

**States:** Vehicle position  $X$  &  $Y$ , Heading angle, Steering angle.

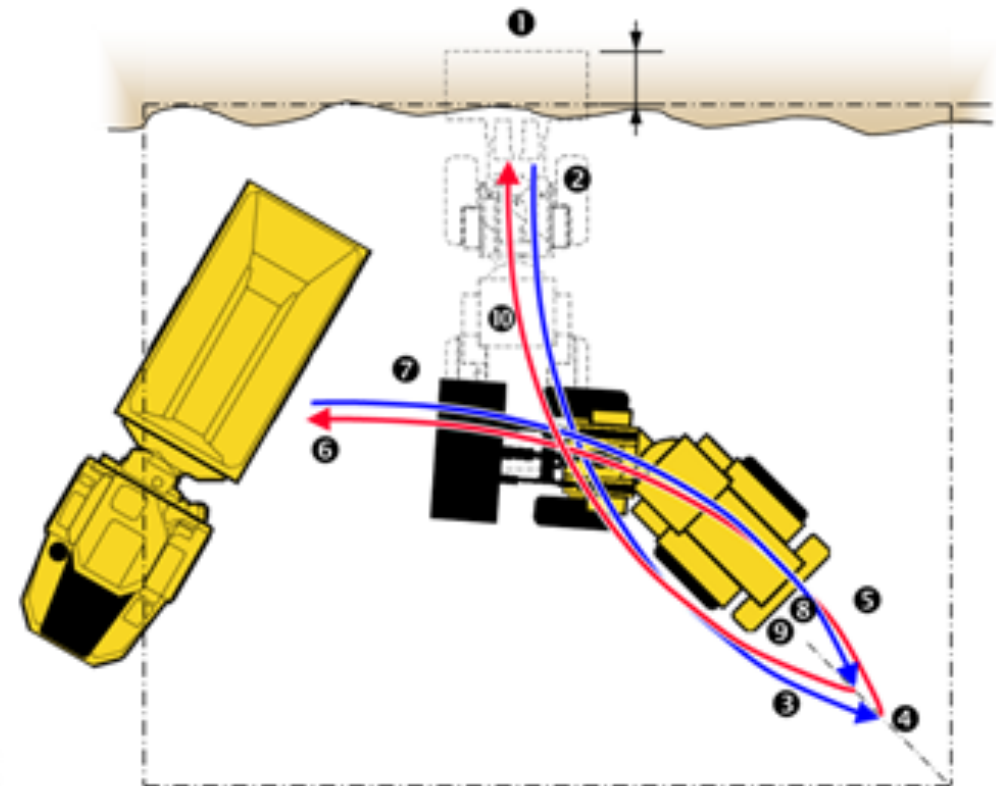
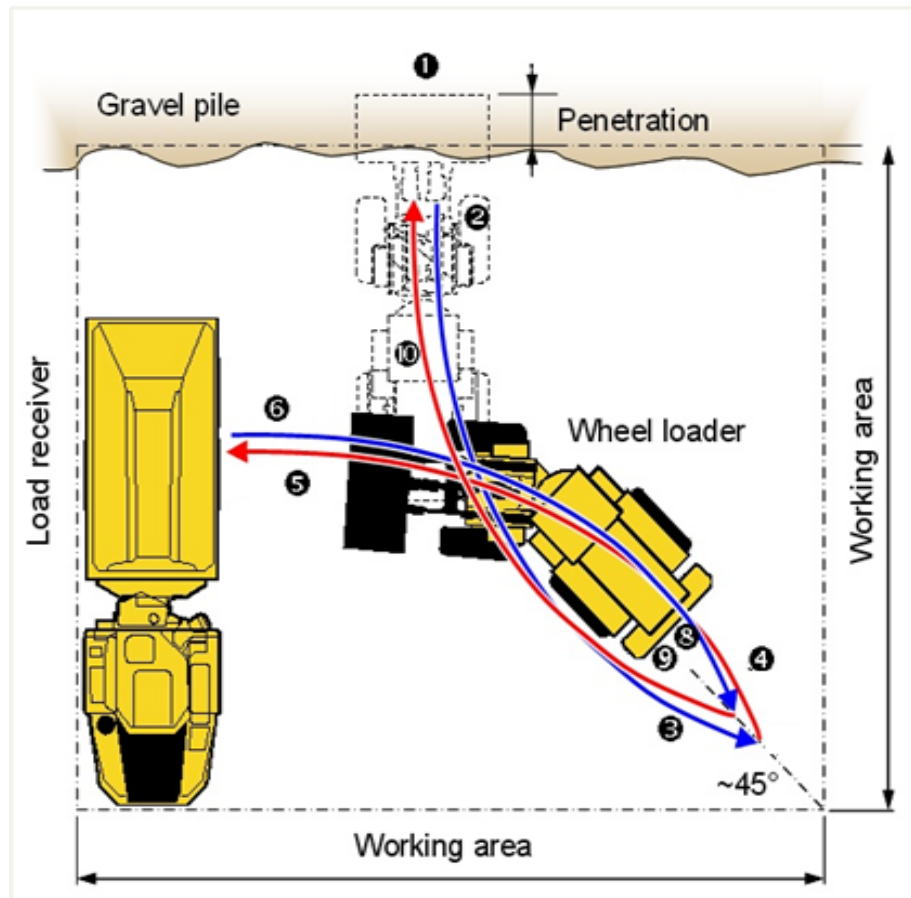
# Trajectory from loading point to load receiver

(Half short loading cycle)

Same trajectory for Min  $M_f$  and Min  $T$  cycles



# Innovation – Changed Driver Instructions



# Outline - Conclusions

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  - Design case – Optimal load receiver placement



# Accomplishing Ground Moving Innovations through Modeling, Simulation, and Optimal Control

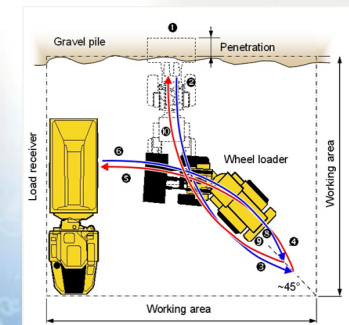
Lars Eriksson, [lars.eriksson@liu.se](mailto:lars.eriksson@liu.se)

Special Thanks to:

Jonas Larsson, PhD, Volvo CE

Anders Froberg, PhD, Volvo CE

Vaheed Nezhadali, PhD Student, Vehicular Systems, LiU



# Publications for futher reading

- **1- Parallel Multiple-Shooting and Collocation Optimization with OpenModelica.** Bernhard Bachmann, Lennart Ochel, Vitalij Ruge, Mahder Gebremedhin, Peter Fritzon, *Vaheed Nezhadali*, Lars Eriksson, and Martin Sivertsson (2012).  
In: Modelica 2012 -- 9th International Modelica Conference. Munich, Germany.
- **2 - Modeling and Optimal Control of a Wheel Loader in the Lift-Transport Section of the Short Loading Cycle.**  
*Vaheed Nezhadali*, and Lars Eriksson.  
In: 7th IFAC Symposium on Advances in Automotive Control. Tokyo, Japan.
- **3 - Optimal Control of Wheel Loader Operation in the Short Loading Cycle Using Two Braking Alternatives.**  
*Vaheed Nezhadali*, and Lars Eriksson.  
In: IEEE VPPC 2013 - The 9th IEEE Vehicle Power and Propulsion Conference. Beijing, China.
- **4 - Optimal lifting and Path Profiles for a Wheel Loader Considering Engine and Turbo Limitations.**  
*Vaheed Nezhadali*, and Lars Eriksson.  
In: Optimization and Optimal Control in Automotive Systems, In Lecture Notes in Control Sciences, Editors: L. del Re, I. Kolmanovsky, M. Steinbuch and H. Waschl. Springer.
- **5- Turbocharger Dynamics Influence on Optimal Control of Diesel Engine Powered Systems.**  
*Vaheed Nezhadali*, Martin Sivertsson and Lars Eriksson  
In: SAE World Congress 2014, Detroit, USA.
- **6 - Wheel loader optimal transients in the short loading cycle.**  
*Vaheed Nezhadali*, Lars Eriksson.  
The 19th IFAC World Congress 2014, South Africa.

# Outline - Conclusions

- Numerical Optimal Control
  - Tools are now mature
  - Solve industrially relevant problems
    - Large size of the state vector
    - Significant nonlinearities
  - Impact on product development beside control
  - Point out counter-intuitive but optimal solutions
- Relevant models, tools, and problems accelerate innovation.

*Thank You for Your Attention!*



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